

Oct 31, 2022

11

Week 9

2020A Adv. Cal. II

Last time we defined

$$\int_{\vec{C}} f ds$$

for a regular parametric curve $\vec{C}(t)$, $t \in [a, b]$, to be

$$\int_a^b f(\vec{C}(t)) |\vec{C}'(t)| dt.$$

Now, we define a curve to be a subset $C \subset \mathbb{R}^2, \mathbb{R}^3$ so that it is the image of a regular parametric curve.

The line integral of f along a curve C is defined to be

$$\int_C f ds = \int_a^b f(\vec{C}(t)) |\vec{C}'(t)| dt.$$

One can see from the Riemann sum approach to the line integral this integral is independent of the choice of the parametrization.

Also, we can add two curves C_1, C_2 together to form $C = C_1 + C_2$ if the endpoints of C_1, C_2 match, that is,

C_1 described by $\vec{C}_1(t)$, $t \in [a, b]$,

C_2 described by $\vec{C}_2(t)$, $t \in [c, d]$,

$$\vec{C}_1(b) = \vec{C}_2(c).$$

Define

$$\int_C f ds = \int_{C_1} f ds + \int_{C_2} f ds.$$

e.g. Evaluate $\int_C (x-3y^2+z) ds$ where $C = C_1 + C_2$,
 C_1 is the line segment bet. $(0,0,0)$ and $(1,1,0)$
 C_2 is - - - - - bet $(1,1,0)$ and $(1,1,1)$

Choose parametrization for C_1 & C_2 :

$$C_1: \vec{c}_1(t) = (0,0,0) + t((1,1,0) - (0,0,0)) \\ = (t, t, 0), \quad t \in [0, 1]$$

$$C_2: \vec{c}_2(t) = (1,1,0) + t((1,1,1) - (1,1,0)) \\ = (1,1,0) + (0,0,t) \\ = (1,1,t), \quad t \in [0, 1]$$

$$\int_{C_1} (x-3y^2+z) ds = \int_0^1 (t-3t^2+0) |\vec{c}'_1(t)| dt \\ = \int_0^1 (t-3t^2) \sqrt{2} dt = -\frac{\sqrt{2}}{2}$$

$$\int_{C_2} (x-3y^2+z) ds = \int_0^1 (1-3+0) \sqrt{1} dt = -\frac{1}{2}$$

$$\int_C (x-3y^2+z) ds = -\frac{\sqrt{2}}{2} - \frac{1}{2} \neq$$

Line integral of a v.f.

$$\vec{F} = (M, N, P) = M\hat{i} + N\hat{j} + P\hat{k} \quad \in \mathbb{R}^3 \\ = (M, N) = M\hat{i} + N\hat{j} \quad \in \mathbb{R}^2$$

Consider a curve from \vec{P} to \vec{Q} , $\vec{c}(t)$, $t \in [a, b]$, $\vec{c}(a) = \vec{P}$,
 $\vec{c}(b) = \vec{Q}$. Define

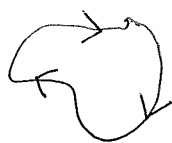
$$\int_C \vec{F} \cdot d\vec{r} = \int_a^b \vec{F}(\vec{c}(t)) \cdot \vec{c}'(t) dt$$

~ When \vec{F} is the force field, $\int_C \vec{F} \cdot d\vec{r}$ gives the work done of \vec{F} along C .

~ $\int_C \vec{F} \cdot d\vec{r}$ is the same as long as the parametrization runs from \vec{P} to \vec{Q} .

~ $\int_C \vec{F} \cdot d\vec{r}$ gets a "-" sign when the parametrization runs from \vec{Q} to \vec{P} .

Thus when we evaluate $\int_C \vec{F} \cdot d\vec{r}$ we need to specify the orientation of the curve. A curve with a specific orientation is called an oriented curve. For a closed curve, the orientation is either anticlockwise or clockwise.



clockwise



anticlockwise.

Another notation

$$\int_C \vec{F} \cdot d\vec{r} = \int_C M dx + N dy + P dz \quad (\mathbb{R}^3)$$

$$= \int_C M dx + N dy \quad (\mathbb{R}^2)$$

e.g. Evaluate $\int_C \vec{F} \cdot d\vec{r}$, $\vec{F} = z\hat{i} + xy\hat{j} - y^2\hat{k}$
 $C, \vec{r}(t) = t^2\hat{i} + t\hat{j} + \sqrt{t}\hat{k}, 0 \leq t \leq 1$

$$\vec{r}'(t) = 2t\hat{i} + \hat{j} + \frac{1}{2\sqrt{t}}\hat{k}$$

$$\vec{F}(\vec{r}(t)) \cdot \vec{r}'(t) = \sqrt{t} \cdot 2t + t^2 \cdot t \cdot 1 - t^2 \cdot \frac{1}{2\sqrt{t}}$$

$$= 2t^{3/2} + t^3 - \frac{1}{2}t^{3/2}$$

$$\therefore \int_C \vec{F} \cdot d\vec{r} = \int_0^1 (2t^{3/2} + t^3 - \frac{1}{2}t^{3/2}) dt = \dots = \frac{17}{20} \neq$$

e.g. Evaluate

4

$$\int_C -y dx + z dy + 2x dz, \quad C = \cos t \hat{i} + \sin t \hat{j} + t \hat{k}$$
$$t \in [0, 2\pi]$$

$$\int_C -y dx + z dy + 2x dz = \int_0^{2\pi} (-\sin t \hat{i} + t \hat{j} + 2 \cos t) \cdot (-\sin t \hat{i} + \cos t \hat{j} + \hat{k}) dt$$
$$= \int_0^{2\pi} (\sin^2 t + t \cos t + 2 \cos t) dt$$
$$= \pi \#$$

Another point of view other than work done.

$$\int_C \vec{F} \cdot d\vec{r} = \int_a^b \vec{F}(\vec{C}(t)) \cdot \vec{C}'(t) dt$$

$$= \int_a^b \vec{F}(\vec{C}(t)) \cdot \frac{\vec{C}'(t)}{|\vec{C}'(t)|} |\vec{C}'(t)| dt$$

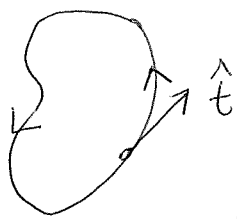
$$= \int_C \vec{F} \cdot \hat{t} ds, \quad \hat{t} = \frac{\vec{C}'(t)}{|\vec{C}'(t)|} \text{ unit tangent}$$

$\vec{F} \cdot \hat{t}$ is the projection of \vec{F} onto the tangential direction of the curve. When \vec{F} stands for the velocity of some fluid, this integral gives the amount of flow along the curve C . When C is a closed one, this flow is called the circulation.

e.g. Find the flow of $\vec{F} = (x, z, y)$ along $\vec{r}(t) = (\cos t, \sin t, t)$
 $t \in [0, \pi/2]$.

$$\text{flow} = \int_0^{\pi/2} (\cos t, t, \sin t) \cdot (-\sin t, \cos t, 1) dt$$
$$= \int_0^{\pi/2} (-\cos t \sin t + t \cos t + \sin t) dt$$
$$= \frac{\pi-1}{2} \#$$

When C is a closed curve in \mathbb{R}^2 running in anticlockwise way, its tangent is



$$\hat{t} = \frac{(x'(t), y'(t))}{\sqrt{x'^2(t) + y'^2(t)}}$$

the unit outer normal

$$\hat{n} = \frac{(y'(t), -x'(t))}{\sqrt{x'^2(t) + y'^2(t)}}$$

The flux of \vec{F} across C is

$$\int_C \vec{F} \cdot \hat{n} \, ds$$

As $\vec{F} = M\hat{i} + N\hat{j}$,

$$\int_C \vec{F} \cdot \hat{n} \, ds = \int_a^b \left(M(\vec{c}(t)) \frac{y'(t)}{\sqrt{\quad}} - N(\vec{c}(t)) \frac{x'(t)}{\sqrt{\quad}} \right) \sqrt{\quad} \, dt$$

$$= \int_a^b M(\vec{c}(t)) y'(t) - N(\vec{c}(t)) x'(t) \, dt$$

$$= \int_C M \, dy - N \, dx,$$

this is another form for the flux.

e.g. Find the flux of the velocity v.f. $(x-y, x)$ across the unit circle $x^2 + y^2 = 1$.

First, we choose $t \mapsto (\cos t, \sin t)$, $t \in [0, 2\pi]$ to parametrize the circle, $\hat{t} = (-\sin t, \cos t)$, $\hat{n} = (\cos t, \sin t)$

$$\text{flux} = \int_0^{2\pi} (\cos t - \sin t, \cos t) \cdot (\cos t, \sin t) \, dt$$

$$= \int_0^{2\pi} \cos^2 t \, dt = \pi. \#$$

(Cont'd)

We recall some definitions.

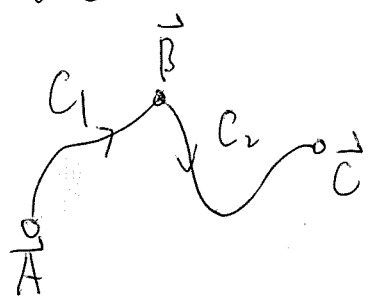
A parametric curve is a map $\vec{c} = [a, b] \rightarrow \mathbb{R}^2, \mathbb{R}^3$ where each components $x(t), y(t), z(t)$ are continuous. It is regular if $x(t), y(t), z(t)$ are continuously differentiable and

$$|\vec{c}'(t)| = \sqrt{x'(t)^2 + y'(t)^2 + z'(t)^2} > 0, \forall t \in (a, b).$$

A curve is the image of some parametric curve. It is a smooth curve if the parametization is a regular one.

Let C_1 be a smooth curve from \vec{A} to \vec{B} , and C_2 a smooth curve from \vec{B} to \vec{C} . Then $C = C_1 + C_2$ is a piecewise smooth curve from \vec{A} to \vec{C} .

$$\int_C \vec{F} \cdot d\vec{r} \stackrel{\text{def}}{=} \int_{C_1} \vec{F} \cdot d\vec{r} + \int_{C_2} \vec{F} \cdot d\vec{r}$$



A vector field $\vec{F} = M\hat{i} + N\hat{j} + P\hat{k}$ is usually defined in an open region. It is usually assumed to be continuous, i.e., M, N, P are continuous functions in the region. It is called a smooth v.f. if M, N, P are continuously differentiable.

x x x

A v.f. \vec{F} in open region G is conservative if there is a function Φ in G s.t. $\nabla\Phi = \vec{F}$, i.e.

$$\frac{\partial\Phi}{\partial x} = M, \quad \frac{\partial\Phi}{\partial y} = N, \quad \frac{\partial\Phi}{\partial z} = P.$$

(When \vec{F} defined in 2-dim, $\frac{\partial\Phi}{\partial x} = M, \frac{\partial\Phi}{\partial y} = N.$) The function Φ is

the potential for \vec{F} .

7

Theorem For a conservative v.f. \vec{F} in G ,

$$\int_C \vec{F} \cdot d\vec{r} = \Phi(\vec{Q}) - \Phi(\vec{P})$$

where Φ is the potential of \vec{F} , C is a ^{piecewise smooth} curve from \vec{P} to \vec{Q} in G .

$$\text{Pf: } \int_C \vec{F} \cdot d\vec{r} \stackrel{\text{def}}{=} \int_a^b \vec{F}(\vec{r}(t)) \cdot \vec{r}'(t) dt \quad \text{when } \vec{r} \text{ is a regular}$$

parametrization of C (assume C to be smooth).

$$\vec{F}(\vec{r}(t)) \cdot \vec{r}'(t) = M(\vec{r}(t))x'(t) + N(\vec{r}(t))y'(t) + P(\vec{r}(t))z'(t)$$

On the other hand,

$$\Phi(\vec{r}(t)) = \Phi(x(t), y(t), z(t)).$$

By the Chain Rule,

$$\begin{aligned} \frac{d}{dt} \Phi(\vec{r}(t)) &= \frac{d}{dt} \Phi(x(t), y(t), z(t)) \\ &= \frac{\partial \Phi}{\partial x}(\vec{r}(t))x'(t) + \frac{\partial \Phi}{\partial y}(\vec{r}(t))y'(t) + \frac{\partial \Phi}{\partial z}(\vec{r}(t))z'(t) \\ &= M(\vec{r}(t))x'(t) + N(\vec{r}(t))y'(t) + P(\vec{r}(t))z'(t) \end{aligned}$$

$$\therefore \int_C \vec{F} \cdot d\vec{r} = \int_a^b \vec{F}(\vec{r}(t)) \cdot \vec{r}'(t) dt$$

$$= \int_a^b \frac{d}{dt} \Phi(\vec{r}(t)) dt$$

$$= \Phi(\vec{r}(t)) \Big|_a^b = \Phi(\vec{r}(b)) - \Phi(\vec{r}(a)) = \Phi(\vec{Q}) - \Phi(\vec{P}).$$

When C is piecewise smooth, for example, $C = C_1 + C_2$, C_1 from \vec{P} to \vec{R} , and C_2 from \vec{R} to \vec{Q} . As both C_1 and C_2 are smooth, by the previous discussion,

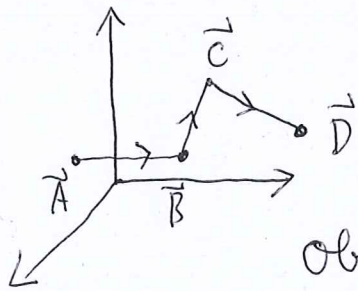
$$\int_{C_1} \vec{F} \cdot d\vec{r} = \Phi(\vec{R}) - \Phi(\vec{P}), \quad \int_{C_2} \vec{F} \cdot d\vec{r} = \Phi(\vec{Q}) - \Phi(\vec{R})$$

$$\begin{aligned} \therefore \int_C \vec{F} \cdot d\vec{r} &= \int_{C_1} \vec{F} \cdot d\vec{r} + \int_{C_2} \vec{F} \cdot d\vec{r} \\ &= \Phi(\vec{R}) - \Phi(\vec{P}) + \Phi(\vec{Q}) - \Phi(\vec{R}) \\ &= \Phi(\vec{Q}) - \Phi(\vec{P}). \quad \# \end{aligned}$$

I forgot to mention in class

e.g. Find the work done of the force $-\frac{g}{z^2} \hat{k}$ along the path

$$C = C_1 + C_2 + C_3$$



C_1 : line from $(1,0,1)$ to $(1,1,1)$

C_2 : line from $(1,1,1)$ to $(1,2,3)$,

C_3 : line from $(1,2,3)$ to $(0,1,\frac{1}{2})$.

Observe that $\vec{F} = 0\hat{i} + 0\hat{j} - \frac{g}{z^2}\hat{k}$ has a

potential $\Phi(x,y,z) = \frac{g}{z}$ in the upper half space.

$$\begin{aligned} \therefore \int_C \vec{F} \cdot d\vec{r} &= \Phi(0,1,\frac{1}{2}) - \Phi(1,0,1) \\ &= \frac{g}{\frac{1}{2}} - \frac{g}{1} = g. \quad \# \end{aligned}$$

Therefore, it is desirable to determine when a v.f. is conservative.

Component Test A v.f \vec{F} is conservative. then

19

$$M_y = N_x, \quad M_z = P_x, \quad N_z = P_y$$

(When $n=2$, $M_y = N_x$)

Pf: If $\vec{F} = \nabla\Phi$, i.e., $M = \Phi_x$, $N = \Phi_y$, $P = \Phi_z$. Then

$$M_y = \Phi_{xy}, \quad N_x = \Phi_{yx}. \quad \text{As } \Phi_{xy} = \Phi_{yx}, \quad M_y = N_x.$$

Similarly, get other 2 relations.

e.g. Is $\vec{F} = xy\hat{i} + y^2\hat{j} + zy\hat{k}$ conservative?

As $M_y = x$, $N_x = 0$, $M_y \neq N_x$, so \vec{F} is not conservative.

e.g. Find (if any) a potential for

$$\vec{F} = (e^x \cos y + yz)\hat{i} + (xz - e^x \sin y)\hat{j} + (xy + z)\hat{k}$$

Component test first.

$$M_y = \frac{\partial}{\partial y} (e^x \cos y + yz) = -e^x \sin y + z$$

$$N_x = \frac{\partial}{\partial x} (xz - e^x \sin y) = z - e^x \sin y. \quad \therefore M_y = N_x.$$

$$M_z = y, \quad P_x = y \quad \therefore M_z = P_x.$$

$$N_z = x, \quad P_y = x \quad \therefore N_z = P_y.$$

\vec{F} passes the component test. Most likely it has a potential.

$$\frac{\partial \Phi}{\partial x} = M = e^x \cos y + yz$$

$\therefore \Phi(x, y, z) = e^x \cos y + xyz + g(y, z)$, g to be determined.

$$\frac{\partial \Phi}{\partial y} = -e^x \sin y + xz + \frac{\partial g}{\partial y}(y, z)$$

$$= N = xz - e^x \sin y \Rightarrow \frac{\partial g}{\partial y}(y, z) = 0, \quad \therefore g(y, z) = h(z)$$

$$\frac{\partial \Phi}{\partial z} = xy + h'(z) = P = xy + z \Rightarrow h'(z) = z, \quad \therefore h(z) = \frac{z^2}{2} + C.$$

Conclusion: $\Phi(x, y, z) = e^x \cos y + xyz + \frac{z^2}{2} + C$, C constant.

110

Remark. There are examples showing that even \vec{F} passes the component test, a potential does not exist. We will discuss more next week.